71

LEVEL BOOK

744

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16.6 in.	21	3.46.6 in.	41	6.76.6 in.	61	10.06.6 in.	81	13.36.6
2	33.0	22	3 63.0	42	6.93.0	62	10.23.0	82	13.53.0
3	49.6	23	3.79.6	43	7.09.6	63	10.39.6	83	13.69.6
4	66.0	24	3.96.0	44	7.26.0	64	10.56.0	84	13.86.0
5	82.6	25	4 12.6	45	7.42.6	65	10.72.6	85	14.02.6
6	99.0	26	4.29.0	46	7.59.0	66	10.89.0	86	14.19.0
7	1.15.6	27	4.45.6	47	7.75.6	67	11.05.6	87	14.35.6
8	1.32.0	28	4.62.0	48	7.92.0	68	11.22.0	88	14.52.0
9	1.48.6	29	4.78.6	49	8.08.6	69	11.38.6	89	14.68.6
10	1.65.0	30	4.95.0	50	8.25.0	70	11.55.0	90	14.85.0
11	1.81.6	31	5.11.6	51	8.41.6	71	11.71.6	91	15.01.6
12	1.98 0	32	5.28.0	52	8.58.0	72	11.88.0	92	15.18.0
13	2.14.6	33	5.44.6	53	8.74.6	73	12.04 6	93	15.34.6
14	2.31.0	34	5.61.0	54	8.91.0	74	12.21.0	94	15.51.0
15	2.47.6	35	5.77.6	55	9.07.6	75	12.37.6	95	15.67.6
16	2.64.0	36	5.94.0	56	9.24.0	76	12.54.0	96	15.84.0
17	2.80.6	37	6.10.6	57	9.40.6	77	12.70.6	97	16.00.6
18	2.97.0	38	6.27.0	58	9.57.0	78	12.87.0	98	16.17.0
19	3.13.6	39	6.43.6	59	9.73.6	79	13.03.6	99	16.33.6
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	16.50 0

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
DRAWING MATERIALS AND SURVEYING INSTRUMENTS

C. HILLCOTHE
ROAD
CHESTER
TWP

B.R. KENNEY
Co. SURVEYOR
CHARDON
OHIO

21

MAY 4 LACKEY GRAU Sanford Cottrel

PLAN ℄ DIA

COUNTY LINE

	0.60	1085.35		1084.75							
260+75					1080.20			17.0	22.5	1	
260				6.55	1078.80	0.0	(F1.5 17.5)	15.0	18.5	(F0.3 19.3)	F0.2
259				8.39	1076.96	F0.4	(F0.1 19.6)	19.0	18.0	(F0.7 18.7)	F0.6
258				10.04	1075.31	F0.6	(F0.8 18.6)	18.0	18.0	(F1.0 18.3)	F0.7
⊙	2.42	1077.12	10.65 w Peg	(1074.70)							
257				3.10	1074.02	F1.3	(F1.4 17.7)	17.3	17.3	(F1.3 17.8)	F1.2
256				4.10	1073.02	F1.3	(F1.5 17.5)	17.3	20.0	(C0.3 20.2)	C0.5
255				4.45	1072.67	F1.9	(F2.1 16.6)	16.5	17.2	F1.5 17.5	F1.6
254				4.70	1072.42	F0.7	(F1.2 18.0)	17.8	23.0	(C 3.2 23.6)	C3.3
+65								20	25.0	(C1.7 21.3)	C1.9
+15					Y.D. O NR			18.0	22.3		
253				4.95	1072.17	F0.5 0.0	(F1.2 18.0)	17.3	18.0	(C1.7 21.3)	
⊙	4.57 2.89	1075.92 1076.45	5.75	1071.37 1073.56							
252				4.37	1072.08	F1.6	(F1.5 17.5)	17.3	17.3	(F1.4 17.7)	F1.5
251				4.13	1072.32	F1.4	F1.3 17.8	17.5	18.3	F1.2 18.0	F0.8

21
12
709

4

		1076.45									
250				3.73	1072.72	F 1.4	(F 1.4 / 17.7)	17.7	18.3	(F 1.0 / 18.3)	F 0.9
249				2.65	1073.80	F 2.4	F 2.3 / 16.4	16.2	17.0	(F 1.7 / 17.2)	F 1.7
248				0.23	1076.22	F 0.1	(F 0.4 / 19.2)	19.2	19.2	(F 0.2 / 19.5)	F 0.2
0	6.07	1082.29	0.33	(1076.12)							
	ON W. peg										
247				3.29	1079.00	C 1.9	C 1.8 / 22.4	21.7	20.5	(C 2.0 / 22.8)	C 2.2
+80					1079.05			~~21.7~~	~~23.0~~		
246				5.55	1076.74	F 0.7	(F 1.4 / 17.8)	17.0	19.0	(F 0.6 / 18.9)	F 0.3
245				8.22	1074.07	F 2.6	(F 2.3 / 16.3)	F 16.0	17.7	(F 1.2 / 18.2)	F 1.2
244				8.25	1074.04	(C 0.4)	(C 0.5 / 20.5)	20.2	19.5	(F 0.3 / 19.3)	F 0.1
243				6.95	1075.34	F 1.1	(F 1.3 / 17.8)	17.5	19.2	F 0.3 / 19.3	F 0.3
⊙	8.96	1083.18	8.07	1074.22							
242				6.54	1076.64	F 0.8	(F 0.8 / 18.6)	18.3	19.5	(0.0 / 19.7)	C 0.1
241				5.34	1077.84	F 1.1	(F 1.3 / 17.8)	18.0	18.2	(F 0.9 / 18.4)	F 0.9
240				3.94	1079.24	C 1.4	(C 1.2 / 21.5)	20.7	20.0	(C 0.2 / 20.1)	C 0.3
BM			2.70	1080.48							
	2.70	1083.11		1080.41							

BT 224 Pt 6960
110.21 Elev

0.8 / 5.5   6.5 / 8.5   ℄

		1083.11									
239				2.57	1080.54	C0.7	(C0.4 / 20.4)	20.0	20.0	(C0.3 / 20.2)	C0.5
238				1.36	1081.75	F0.3	(F0.5 / 19.0)	18.7	18.3	(F0.9 / 18.4)	F0.8
				604							
237				.72	1082.39	F0.4	(F0.6 / 18.9)	19.0	18.0	(F1.2 / 18.0)	F1.1
⊙	ON E peg 7.6	1088.43	(1.84)	1081.27							
236				5.49	1082.94	F1.4	(F1.1 / 18.1)	18.4	17.7	(F1.4 / 17.7)	F1.3
235				4.85	1083.58	F1.2	F1.1 / 18.1	18.2	17.5	(F1.2 / 18.0)	F1.4
234				4.04	1084.39	F1.2	(F1.2 / 18.0)	18.0	18.2	(F1.1 / 18.1)	F1.0
~~+50~~					~~1084.87~~						
233				3.05	1085.38	F1.1	(F1.4 / 17.3)	17.5	18.5	(F0.5 / 18.6)	F0.4
+50					~~1085.94~~						
232				1.89	1086.54	F0.2	(F0.3 / 18.9)	19.0	19.2	(F0.2 / 19.1)	0.0
~~+50~~				~~1.26~~	~~1087.17~~						
231				64	1087.99	F0.3	(F0.5 / 19.9)	19.0	18.5	(F0.8 / 18.2)	F0.4
⊙	W. 8.62 peg	1096.08	0.97	1087.46							
+50			~~7.66~~		1088.42						
230				7.04	1089.04	F1.0	F1.0 / 18.3	18.2	18.0	F1.2 / 17.6	F1.0
~~+50~~					~~1089~~.67						

Sub Elev 1.2 + 21 = ... from dist

1096.08

229			5.79	1090.29	F0.7	(F0.7 18.2)	18.7	18 0	(F1.0 17.9) F0.9
+50				~~1090.92~~					
228			4.54	1091.54	F1.0	(F1.1 18.1)	18.2	18 0	(F0.8 18.2) F0.9
+50				~~1092.17~~					
227			3.29	1092.79	F1.1	(F1.1 18.1)	18 0	18 0	(F0.8 18.2) F0.8
+50			~~2.56~~	1093.52					
226			1.65	1094.43	C0.5	(C0.6 20.7)	19.5	18.3	(F0.9 18.0) F0.7
⊙		1.15	1094.93						
+50	9.77	1104.70		1095.54					
225			7.86	1096.84	C0.3	C0.2 20.1	20 0	19 0	(F0.3 19.3) F0.3
224			5.06	1099.64	C0.4	C0.5 20.5	18.7	18.4	(F0.8 18.6) F0.8
223			2.18	1102.52	F1.4	(2.2 16.4)	16.4	19.0	(F0.3 19.3) F0.2
⊙	10.90	1013.54							
222		2.06	1012.64	1107.12	F2.7 2-1	(F2.7 16.6) F 2-1	19.0	21.0	(C1.4 21.8) C1.5

Hp. Sta 222

6.42

LACKEY
GRAU
PHILIPS

		1013.54								
				13.13						
221				11.12	1112.42	F2.9	(33.17.6)	19.5	22.4	(C2.1 22.9)	C2.4
⊙	12.11	1025.55	0.10	1013.44						
220			.83	.783	1117.72	F1.8	[F3.2 17.3] 2-1	16.0	22.6	(C2.1 22.9)	C2.4
219			2.50	2.53	1123.02	C2.2	(C2.0 22.7)	22.7	22.0	(C1.5 22.0)	C1.6
⊙	11.76	1037.12	0.18	1025.36							
218				8.80	1128.32	C0.9	(C0.8 21.0)	21.0	21.7	(C1.4 21.8)	C1.5
	from Bm	1041.74									
217				3.50	1133.62	C2.8	(C2.5 23.5)	23.0	23.0	(C2.7 23.8)	C2.9
⊙	4.97	1041.66	0.43	(1036.69)							
+25		210		5.21	1136.53	C1.7	C1.6 22.2	21.5	24.0	(C3.0 24.3)	C3.1
		1035.56									
216				4.71	1137.03	C0.3	(C0.2 20.1)	20.0	22.0	(C1.6 22.1)	C1.7
215				4.38	1137.34	F2.5	(F2.5 16)	15.2	18.0	(F1.4 17.7)	F1.2
214				2.94	1138.80	F1.6	(F1.8 17.1)	17.0	18.0	(F1.1 18.1)	F1.2
⊙	6.87	1046.85	1.78	1039.96							
213				C.35	1140.50	C0.1	(F2.0 19.5)	19.4	22.0	(C1.4 21.9)	C2.0
~~15~~								22.5	23.5		
212				5.53	1141.32	C1.9	(C1.6 22.2)	22.0	23.0	(2.8 24.0)	C3.1
+60								19.7	22.2		
211				6.45	1140.40	F0.7	(F0.8 18.6)	17.5	19.7	(C0.5 20.5)	C0.6
210				8.25	1138.60	F1.8	(F2.0 16.7)	16.5	18.0	(F0.5 19.0)	F0.3
209				10.05	1136.80	F1.8	(F1.9 16.9)	17.0	19.6	(F1.1 18.2)	F0.3
⊙	5.39	1040.53	11.71	1035.14							

6.8
C.2
25

1040.53

208			~~11.5.28~~	1135.25	F 1.8	(F 1.8 / 17.1)	17.0	18.0	(F 1.1 / 18.1)	F 0.6
207 BM	578 / 1039.75		5.30	1135.23	F 1.9	(F 2.0 / 16.7)	16.7	19.0	(F 0.6 / 18.9)	F 0.3
206			5.20	1135.33	F 0.8	(F 1.0 / 18.4)	19.5	22.0	(C 1.6 / 22.1)	C 1.7
+75			5.54	1134.99	C 0.4	F 0.2 / 20	21.5	16.7	C 1.3 / 21.7	C 1.5
+40						F 1.6 / 17.4	13.5	17.0		
205				1132.52			13.3	16.0		
+50			10.01 .23	1130.52	F 1.5	(F 1.5 / 17.5)	17.5	17.7	(F 1.6 / 17.4)	F 1.6
⊙		11.50	1029.03							
204	NW 7.03 W Pg 1036.06		6.76	1129.30	F 0.4	(F 0.6 / 18.9)	18.2	19.0	(F 1.1 / 18.1)	F 1.0
203			5.34	1130.72	F 1.4	(F 1.7 / 17.2)	17.3	17.5	F 1.7 / 17.2	F 1.6
202			2.99	1133.07	F 2.5	(F 2.5 / 16.0)	16.0	21.5	~~NT~~ 2 0.5	C 1.5
201			.36	1135.74	F 3.0	(F 2.4 / 16.2)	16.0	20.0	(C 0.2 / 20)	C 0.1
200			1.80	1135.56	F 2.5	(F 2.2 / 16.5)	16.3	18.5	(F 0.8 / 18.6)	F 0.6
⊙	10.55	1046.36	0.25	1035.81						

104636

199				4.98	1141.38	F2.6	(F2.4 / 1.3)	16.0	20	(C0.2 / 20)	C0.2
198				9.12 / 2.16	1144.20	F1.4	(F1.2 / 18)	17.5	23.0	C2.4 / 23.4	C2.6
⊙	7.22 / 1.89	105332 / 105343	026	1046.10	1151.53						
197				6.40	1147.02	F0.7	(F0.6 / 18.9)	18.5	26.2	(C4.0 / 25.8)	C4.5
+40				5.12	1148.30	F0.2	(F0.1 / 19.6)	19.0	24.0	(C3.1 / 24.4)	C3.3
196				4.93	1148.49	F0.8	(F0.7 / 18.7)	18.2	23.0	(C2.3 / 23.1)	C2.5
195				5.41	1148.01	F1.4	(F1.4 / 17.7)	17.5	21.0	C1.3 / 21.7	C1.5
194				5.63	1147.79	F1.7	F1.5 / 17.5	17.5	17.5	F1.1 / 18.1	F0.8
193				5.27	1148.15	F1.8	(1.9 / 16.9)	16.5	21.3	C0.9 / 20.9	C1.2
192				4.35	1149.07	F2.3	(F2.1 / 16.6)	16.5	17.2	F1.6 / 17.9	F1.4
⊙	12.43	106102	4.83	1048.59							
191				10.45	1150.57	F1.6	(F1.5 / 17.5)	17.0	18.2	(F0.9 / 18.4)	F0.6
190				7.26	1153.76	F1.6	(F2.1 / 16.6)	15.0	17.2	(F1.3 / 17.8)	F0.6

106.102

189				17.52 2.66	1158.36	C1.7	(C1.7 22.2)	22.0	26.5	(C4.9 26.9)	C5.1
⊙	13.07	107.2.88	1.21	1059.81							
188				10.03	1162.85	C1.1	(C1.1 21.4)	20.5	22.5	(C2.1 22.9)	C2.2
187				6.33	1166.55	F0.8	(F 1.5 17.5)	18.0	21.0	(C1.0 21.3)	C1.1
186				3.42	1169.46	C0.6	(C0.5 20.5)	20.0	20.5	(C0.5 20.8)	C0.9
185			3.76	1.42	1171.46	C0.8	(C1.0 21.2)	20.7	23.0	(C3.0 C1.3 21.7)	C1.4 C2.1
⊙	3.14	107.5.2 3.22	0.90	1071.98							
84 +25		107.19.0		3.31	1171.91	C2.5	C2.5 C1.5 22.0	22.6	22.2	(C1.9 22.6)	
184				3.36	1171.86	C1.5 C2.5	C2.3 C1.4 21.8	22.5	22.0	(C1.7 C1.0 21.3)	C1.0 C1.8
BM	1.31	107.41.2		1072.21							
183	Re Stamp			3.46	1170.64	F0.8	F0.9 18.4	18.0	16.5	(F 2.0 1.6.8)	F1.8
182				5.23	1168.89	F1.5	F1.5 17.5	17.3	17.0	(F 1.7 17.3)	F1.6
181				5.62	1168.50	F2.1	F2.1 16.6	16.4	15.0	(F 2.5 15.0)	F2.5
⊙	4.51	1072.6.0	6.03	1068.09							
180				4.26	1168.34	F2.1	F2.0 16.7	16.7	16.2	(F 2.5 16)	F2.3
179				4.12	1168.18	F1.4	F1.4 17.6	18.7	17.8	(F 1.4 17.7)	F1.6

929
704
2,20

℄

		1072.60									
178				4.58	1168.02	F0.1	(F0.4 19.2)	19.0	19.5	(F0.4 19.2)	F0.3
177+50				~~4.66~~	1167.99			20.8	20.3		
177				4.82	1167.78	C1.4	(C1.3 21.7)	21.5	19.5	(C0.4 20.4)	C0.5
⊙ ⊗	1.02 on W. Pg	1070.21	3.41	1069.19							
176			4.62		1165.59	C1.9	(C1.9 20.4)	1-1 20.4	1-1 16.0	(F0.4 18.1)	C0.6
175			9.29		1160.82	C2.4	(C2.3 20.8)	1-1 20.3	1-1 20.0	(C1.2 19.2)	C2.2
⊙	2.41	1062.93	(9.69)	1060.52							
+65					1158.89			1-1 22.0	1-1 20.9		
174			7.62		1155.31	C4.5	(C3.8 22.3)	1-1 21.0	1-1 22.0	(C1.5 20)	C2.0
⊙	2.56	1052.49	13.00	1049.93							
173				2.79	1149.70	C0.5	(C0.2 18.7)	1-1 20.3	1-1 21.0	(3.1 17.2)	(2-1) F 2.8
⊗											
172				7.73	1144.76	F2.4	(F2.3 16.4)	18.3	19.0	(F2.0 16.8)	F2.0
171				9.34	1143.15	F1.3	(F1.4 17.6)	17.5	18.0	(F1.0 18.3)	F1.1
170				7.53	1144.96	F0.5	(F0.8 18.6)	18.5	18.2	(F1.2 18.0)	F1.0
⊙	10.56	1056.93	6.12	1046.37							
169	drip 3' Rock			9.43	1147.50	C0.8	(C0.4 20.4)	20.4	16.2	(F1.6 17.4)	F0.6

1046.37 on Rock at 169+

105693

				5.47	1151.46
168					
⊙	1145	1067.00	1.38	1055.55	
	12.54	1068.09			1155.66
167	super El. in curve			11.34	
166	4.2 / 1.2 / 5.4 / 27 / 81 Less ds on Cut			7.14	1159.86
0					
165+50				5.04	1161.96
165				4.03	1164.06
⊙				11.90	
				9.80	
164+50				1.93	1166.16
⊙	9.21	1075.96	1.34	1066.75	
		124			
164	BM	1074.72		7.70	1168.26
+50				5.65	1170.31
163			3.1 / 9 / 22	3.97	1171.99
162				1.86	1174.10
				3.13	
161+25					1174.21
⊙	3.03	1077.34	1.65	1074.37	
161				3.40	1173.94

27 25 ℄

1344
1134
1.80

1.6	F 1.6 / 14.4	20.5	18.0	(F 1.0 / 18.3)	F 0.8
F 1.8	(F 2.7 / 16.3)	F 16.0	24.2	(C 2.9 / 23.9)	C 3.1
C 0.5	(C 0.5 / 20.5)	20.4	25.0	(C 4.1 / 25.1)	C 4.2
C 0.1	(C 0.1 / 20)	20.0	24.0	(C 3.5 / 24.2)	C 3.8
C 1.6	(C 1.6 / 22.1)	22.0	25.3	(C 4.4 / 25.6)	C 4.6
C 1.5	C 1.4 / 21.8	21.7	26.3	(C 4.9 / 26.3)	C 5.0
C 0.3	C 0.6 / 20.6	20.0	23.5	(C 3.2 / 23.8)	C 3.5
F 0.7	(F 0.7 / 18.7)	18.5	19.0	(F 0.2 / 18.4)	F 0.1
F 1.2	(F 1.3 / 17.7)	17.8	17.5	F 1.4 / 16.9	F 1.2
C 0.6	(C 0.6 / 20.6)	20.0	19.0	(0.0 / 19.7)	C 0.4
C 2.0	C 1.6 / 22.2	22.2	23.0	(C 2.0 / 22.7)	C 2.2
C 2.5	(C 2.2 / 23.2)	22.8	22.0	(C 1.7 / 22.3)	C 1.7

107734

160+60						
160				6.0	1171.34	
159				9.30	1168.04	
				12.05	1165.29	Mail Box
0		2.74	1168.03			
158				3.29	1164.74	
157				6.59	1161.44	
	⊙	3.88	1160.91	11.00	1157.03	
156			5.1.17	2.77	1158.14	
155+25				5.25	1155.66	
155				6.07	1154.84	
154				9.27	1151.64	
0		3.32 / 11.43	1155.56 / 1163.67	8.67	1152.24	T.B.M.
153				3.79	1151.77	
152				6.97	1156.70	
0		5.[illegible]	1168.58	0.41	(1163.26)	
151				5.38	1163.20	
0		12.50	1180.66	0.42	1168.16	
50+50					1166.45	

1/9

C 2.4	(C 2.0 / 22.7)	23.0	21.0	(C 0.8 / 20.8)	C 1.1
C 1.5	(C 0.1 / 21.3)	21.2	18.3	(F 0.4 / 19.2)	F 0.1
C 3.2	C 3.0 / 24.3	24.2	22.0	(F 0.4 / 19.2)	F 0.2
C 1.1	(C 0.9 / 20.9)	21.2	18.2	(F 0.7 / 18.7)	F 0.7
C 3.4	C 3.0 / 24.2	24.2	20.4	(C 0.6 / 20.6)	C 0.7
C 4.7	(C 4.6 / 26.6)	26.3	21.5	(C 1.9 / 22.5)	C 2.2
F 0.3	(F 0.5 / 19.0)	19.0	23.5	(C 2.4 / 23.3)	C 2.5
2 F 2.1	(F 2.2 / 16.5)	21.0	21.0	(19/19.1 / 2 ft d)	F 1.7
F 2.1	(F 1.5 / 17.5)	21.0	19.3	F 2.5/17.0 / 2 ft di	F 2.5
2 / 4.0	(F 4.0 / 9)	23.0	22.0	(2' d / F 2.0 / 18.5)	F 2.1 / F 2.1
2 F 2.5	F 3.9 / 19.3	1-1 / 21.3	1½-1 / 20.0	(C 1.0 / 21.2)	C 1.2

[illegible] 2-1 slope — See plan

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PHILIPS } MAY 11

1180.66

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8.8
14.2

150				10.96	1169.70	c8.0	c8.0 26.5	1-1 26.4	See plan	(c8.6 22.8)	c8.8 See plan
⊙	3.55	1183.96	0.25	1180.41							
	turn lip rock s of drive										
149			7.84		1176.12	c6.3	(c5.4 23.9)	24.0	"	(c3.8 18.0)	c4.0
148+50			~~3.20~~		1178.76			24.0	21.0	~~(c0.9 17.7)~~	~~c1.0~~
148			3.17		1180.79	0.0	c0.2 20	20.0	19.0	0.0 19.7	0.0
147			.88		1183.08	F1.3	F1.5 17.5	17.0	Fill 15.0	(F1.8 17.1)	F1.4
⊙	8.08	1191.09	0.95	1183.01							
146	BM	0.78 87.31 ✓	6.41		1184.68	c0.8	(c0.6 20.7)	20.5	17.0	(F1.6 17.4)	F1.4
145			5.09		1186.00	c2.1	(c1.9 22.6)	21.5	19.3	(c0.2 20.1)	c0.6
144			4.31		1186.78	F1.0	(F1.1 18.1)	18.0	18.0	(F1.7 17.2)	F1.4
143			3.81		1187.28	F0.8	(F1.0 18.3)	18.3	16.0	(F2.0 16.7)	F1.4
142			3.21		1187.88	F0.5	(F0.7 18.7)	19.0	17.0	(F1.7 17.3)	F1.3
141			2.41		1188.68	F1.4	(F1.7 17.1)	17.0	16.4	(F2.0 16.7)	F1.9
140			6.47		1189.58	F2.6	F2.4 16.3	17.0	16.7	(F2.0 16.7)	F1.9
⊙	8.10	1196.05	3.14	1187.95							

			1196.05						
139				5.57	1190.48				
138+50				5.12	1190.93				
138				4.67	1191.38				
137				3.77	1192.28				
136				2.87	1193.18				
135				1.97	1194.08				
134				1.07	1194.98				
⊙	4.91	1200.39	0.57	1195.48					
		379							
		1196.60							
133				4.51	1195.88				
132	8.67	1205.53	BM	3.61	1196.78				
				1196.66					
131				7.65	1197.68				
130				6.52	1198.81				
129				4.92	1200.41				

C0.3	(C0.2 20.1)	20.3	16.5	(F0.7 19.7)	F0.5	17 dia			
C1.0	(C1.0 21.3)	21.3	15.0	F (F2.5 16.0)	F2.3				
F0.8	(F0.9 18.9)	18.5	16.0	(F2.7 16.0)	F1.8				
F1.8	(F2.0 16.8)	17.0	17.7	(F1.4 17.7)	F1.8				
F2.1	(F2.3 16.4)	17.0	17.0	(F1.8 16.9)	F1.5				
F1.0	(F1.0 18.3)	18.2	16.4	(F2.2 16.6)	F2.0				
F1.4	(F1.5 17.5)	17.5	16.2	(F2.3 16.3)	F1.8				
F1.3	(F1.4 17.7)	18.0	18.2	(F1.0 18.3)	F0.6				
F1.6	(F1.4 17.7)	18.2	19.0	(F0.5 19.0)	F0.3				
F0.6	(F0.7 18.7)	19.0	18.4	(F1.0 18.3)	F0.8				
F0.6	(F1.0 18.3)	18.5	16.6	(F1.8 17.1)	F1.5				
F0.1	(0.0 19.7)	19.5	16.3	(F2.2 16.5)	F2.1				

33.6
12.6
21.0

		1205.33									
128				3.09	1202.24	F0.5	(F0.7 18.7)	18.2	F 15.0	(F2.5 16.0)	F2.3
127				1.26	1204.07	F1.0	F1.2 18.0	17.2	19.5	(F2.8 17.2)	F2.1
⊙	9.53	1214.80	0.06	1205.27							
126		38 r 121 092		8.90	1205.90	F1.6	(F1.8 17.1)	17.2	19.2 2-1 fw	F1.7 18.3	F1.5
125				7.07	1207.73	F1.7	(F 1.7 17.1)	17.0	19.0	(F2.0 16.8)	F1.7
124+30											
124+10				5.42	1209.38	C0.9	(C0.8 21.0)	~~20.3~~	F	C0.3 20.2	C0.6 [illegible] 3' back
							See plan				
124				5.24	1209.56						
123				3.41	1211.39	C0.6	(C0.6 20.6)	20	18.0	(F0.8 18.6)	F0.5
122				1.58	1213.22	F0.3	(F0.4 19.1)	19	18	(F1.1 18.1)	F1.2
⊙	11.65	1225.50	0.95	1213.85							
121				10.04	1215.46	F0.2	F0.4 19.2	19.2	17.4	(F1.4 17.6)	F1.2
120				6.99	1218.51	F0.1	F0.2 19.5	19.0	17.0	(F1.5 17.5)	F1.2
119				3.53	1221.97	C2.0	C1.7 22.3	21.5	17.5	(F1.4 17.7)	F0.7
⊙	7.36	1232.11	0.75	1224.75							
118				6.68	1225.43	C2.2	C1.9 22.6	22.2	19.0	F0.4 19.1	F0.2

Sta	BS	HI 123211	FS	Elev
117			4.75	227.36
116			4.35	227.76
115			3.72	228.39
114			1.70	230.41
⊙	11.66	242.84	0.93	(231.18)
113	BM	242.69	10.18	232.66
112			7.93	234.91
111			5.68	237.16
110			3.43	239.41
109			1.18	241.66
⊙	11.51	253.79	0.56	242.28
108			9.88	243.91
107			7.63	246.16

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F0.3	(F0.3 19.3)	19.4	20.2	(C0.5 20.5)	C0.6
F2.5	(F2.3 16.0)	16.2	16.0	(F2.2 16.5)	F2.3
F1.5	(F1.6 17.4)	17.3	16.0	(F2.5 16.0)	F2.4
F1.0	(F1.3 17.8)	17.7	18.5	(F0.4 19.2)	F0.3
C0.8	(C0.7 20.8)	20.5	20.2	(C0.7 20.8)	C0.7
F0.1	(F0.4 19.2)	19.2	19.6	(OD 19.7)	C0.4
F1.5	(F1.6 17.4)	17.5	17.6	(F1.0 18.3)	F0.9
F1.5	(F1.7 17.2)	17.5	16.5	(F2.2 16.5)	F1.5
F1.4	(F1.7 17.2)	17.0	18.5	(F0.5 19.0)	F0.4
F0.9	(F1.0 18.3)	18.2	19.0	(F0.4 19.1)	F0.2
C0.9	(C0.6 20.7)	20.5	20.5	(C1.0 21.2)	C1.1

		1253.79		
106			5.38	1248.41
105	12.54	1266.15	2.58	1251.21
⊙			0.18	1253.61
104	Top Large Rock S. of School [illegible]		11.03	1255.12
103			6.57	1259.58
102			2.11	1264.04
⊙	4.58	1270.39 4.07 1266.32	0.34	1265.81
101			2.72	1267.67
+75			2.64	1267.75
100			4.89	1265.50
99+70			6.54	1263.85
+25			9.02	1261.37
⊙	0.13 5.55	1257.60 1263.42	12.92	1257.47
99				1260.00
98	0.01	1257.48	2.98	1254.50

C1.3	(C1.2 21.6)	20.8	17.5	(F1.4 17.7)	F 1.2
F0.5	(F0.5 19.0)	18.7	16.6	(F1.9 16.9)	F2.0
F0.2	(F0.5 19.0)	18.5	18.0	(F1.0 18.3)	F1.0
F0.3	(F0.4 19.2)	20.3	20.9	(0.0 19.8)	C0.1
F0.6	(F1.0 18.3)	18.0	19.0	(F0.3 19.3)	F0.1
F0.1	(C0.2 20)	19.0	19.8	(C0.1 19.9)	C0.2
C0.3	(C0.1 19.9)	19.7	19.0	(C0.1 19.9)	C0.2
C2.8	(C2.5 23.5)	23.0	18.5	(F0.3 19.3)	F 0.1
C3.6	(C3.5 25.0)	25.2	19.5	(C0.2 20)	C0.3
~~C1.2~~	~~(C1.6 21.3)~~	22.0	~~21.0~~	(C0.6 20.7)	~~C0.5~~
C3.0	C 3.0	24.3	21.0	C0.4	
C2.9	(C2.8 23.9)	24.0	15.4 F	(C 1.1 18.1)	C 0.4

25

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		125748								
97			8.48	1249.00	C1.1	(C1.1 21.4)	21.5	18.7	(F1.0 18.3)	F0.7
⊙	0.16	1244.96	12.68	1244.80						
96			.65	1244.31	F0.3	(F0.3 19.3)	19.5	18.5	(F0.7 18.7)	F0.5
95			3.71	1241.25	F0.3	(F0.7 18.7)	20.3	18.8	(F0.8 19.3)	F0.2
94			5.96	1239.00	F1.2	(F1.2 18.0)	17.7	17.7	(F0.9 18.4)	F0.7
93			8.21	1236.75	F1.3	(F1.4 17.7)	17.3	19.0	(F0.3 19.3)	(C0.2)
92			10.31	1234.69	F0.6	(F0.6 18.9)	18.5	20.0	(C0.3 20.2)	C0.6
⊙	0.12	1235.90 5.45	9.18	1235.78						
91	Correct NI	1230.55 1235.94	2.90	1233.00	F0.5	(F0.5 19.0)	19.0	18.7	(F0.5 19.0)	F0.3
90			4.40	1231.50	F0.8	(F0.8 18.6)	18.7	18.7	(F0.4 19.1)	0.0
89			5.94	1230.00	C0.3	(C0.2 20.1)	20.3	18.0	(F1.1 18.1)	F0.8
88			7.52	1228.42	F0.3	(F0.5 19.0)	19.4	18.0	(F1.1 18.1)	F1.0
⊙	0.23	1228.26	7.87	1228.08						
87			2.01	1226.25	C0.5	(C0.4 20.4)	20.0	19.7	(C0.4 20.4)	C0.6
86			4.84	1223.42	C0.6	C0.5 19.0	20.4	19.7	(C0.6 20.7)	C0.9

67
47
20

1228.26

85			8.05	1220.21	C0.4	(C0.2 / 20.0)	20.0	19.4	(F0.2 / 19.6)	C0.1
84			10.12	1218.14	F0.4	(F0.4 / 19.2)	19.0	21.0	(F0.3 / 19.3)	F0.1
⊙	0.67	1217.23	11.70	1216.56						
83		0.36 / 1216.87	0.95	1216.28	C1.4	(C1.4 / 21.9)	21.5	21.0	(C0.4 / 20.4)	C0.5
82		1217.23	2.81	1214.42	F0.3	(F0.2 / 19.6)	21.0	21.0	(C0.3 / 20.3)	C0.4
81			4.67	1212.56	F1.1	F1.6 / 17.4	17.0	23.0	(F1.9 / 17.1)	F1.6
80+30							19.0	20.0		
80	See Plan		6.67	1210.56	F1.2	(F1.3 / 17.9)	See Plan		(F2.5 / 19.4)	(special d) F2.6
79			9.47	1207.76	F2.1	(F2.1 / 16.6)	16.5	20.5	(F2.0 / 19.9)	special d F2.0
⊙	7.83	1215.45	9.61	1207.62						
78			8.80	1206.65	F1.4	F2.7 (2.1) / 16.5	16.0	17.0	(F1.6 / 17.4)	F1.6
77			8.01	1207.44	C1.2	C0.9 / 21.1	20.1	18.0	(F1.4 / 17.7)	F1.4
76			5.77	1209.68	C2.6	C2.5 / 18.5	18.0	17.4	F1.4/17.7 See Plan	F1.1
75			3.52	1211.93	C3.5	C3.5 / 25.0	24.5	20.0	C0.2 / 20.0	C0.4
⊙ BM	2.01	1216.33	1.10	1214.35 / 1214.32 com						

63
47

637
.67
17

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		121633						
74		3.33/213.00		C0.4	(C0.4 20.4)	20.5	20.5	C0.2 20.0	C0.7
73		3.87/212.46		F1.2	(F1.2)	17.3	17.0	(F1.7 17.2)	F1.8
72		4.66/211.67		F1.5	(F2.7 16.6)	17.5	16.5	(F2.1 16.6)	F2.1
71		4.21/212.12		0.0	(0.0 19.7)	19.4	19.5	(0.0 19.7)	C0.2
70		3.55/212.78		F0.1	0.0 19.7	19.7	19.0	(F0.2 19.5)	F0.2
69		2.89/213.44		F0.7	(F0.7 18.7)	18.5	19.0	(F0.6 18.9)	F0.6
68		2.23/214.10		F0.4	(F0.5 19.0)	19.0	19.5	(F0.2 19.5)	F0.1
ⓒ	2.47	216.88	1.92 12441						
67		2.25/214.63		F1.1	F1.3 17.8	18.0	17.4	(F1.5 17.5)	F1.4
66		2.52/214.36		F0.7	F1.0 18.3	18.2	18.4	(F1.6 17.4)	F1.5
65		2.92/213.96		F0.9	F1.0 18.3	18.2	17.6	(F1.7 17.2)	F1.6
64		3.32/213.56		F0.7	F0.7 18.7	19.0	17.4	(F1.7 17.2)	F1.6
63		3.84/213.04		F0.3	F0.5 19.0	19.5	18.0	(F1.0 18.3)	F1.0

121688

62			5.17	1211.71
TBM spike in tele pole	0.0	1213.58	3.30	1213.58
61+75			2.34	1211.24
61			4.14	1209.44
60			7.22	1206.36
BM			6.80	120.678 ✓
59			9.57	1204.01
⊙	2.26	1204.76	11.08	120 250
58		2.25	~~11.0~~	1202.51
57			3.75	1201.01
56			4.20	1200.56
55			2.55	1202.21
⊙	5.96	1210.32	0.40	1204.36
54			5.41	1204.91
53			2.71	1207.61
52+50			2.11	1208.21
BM			3.10	1207.20

C1.4	(C1.2 / 21.5)	21.5	20.0	(C0.4 / 20.4)	C0.6
		~~21.7~~	~~18.5~~		
C1.7	(C1.9 / 22.6)	22.5	19.7	(C0.1 / 19.7)	C0.3
C1.4	C1.3 / 21.7	21.5	19.0	(F0.4 / 19.2)	F0.1
F0.3	(F0.3 / 19.3)	19.0	18.0	(F1.3 / 17.8)	F1.2
F1.9	(F1.9 / 16.9)	17.4	17.0	(F1.7 / 17.1)	F1.7
F1.6	(F1.6 / 17.4)	17.0	17.2	(F1.4 / 17.7)	F1.5
F1.0	F1.0 / 18.3	18.0	17.0	(F1.5 / 17.5)	F1.2
C1.2	(C1.1 / 21.4)	20.2	18.0	(F1.1 / 18.1)	F0.7
C0.4	(C0.3 / 20.2)	20.0	18.5	(F0.7 / 18.7)	F0.6
C0.5	(C0.5 / 20.5)	19.2	19.5	(F0.2 / 19.5)	F0.1
C0.2	(C0.1 / 19.9)	20	20.0	(C0.1 / 19)	C0.2

		1210.32			
52			3.02	1207.30	
51			6.34	1203.98	
50			9.66	1200.66	
⊙	0.09	1197.64	(12.77)	1197.55	
49		.30	~~1?.98~~	1197.34	
48			3.42	1194.22	
47			6.14	1191.50	
46			8.66	1188.98	
⊙	1.26	1187.32	11.58	1186.06	
45		11.28 11.18	11.18 .86	1186.46	
44		11.5 11.2	338 ~~[illegible]~~	1183.94	
43			5.97	1181.35	
42			8.70	1178.62	
41		1174.91	11.57	1175.75	
⊙	4.95	1179.33	12.94	1174.38	DM
40	0.53	~~1178.67~~	~~5.93~~ 2.21	1172.74	<1178.14

5.65
5.05
.60

565

C0.5

C

F0.4	(F0.5 19.0)	19.0	21.0	(C1.0 21.3)	(C1.1
F1.0	(F0.7 18.7)	18.5	20.7	(C0.6 20.7)	(C0.8)
0.0	(0.0 19.7)	19.9	20.0	(C0.4 20.3)	C0.5
F1.8	(F2.4 16.1)	16.0	20.2	C0.5 20.5	C0.8
F1.3	(F1.3 17.8)	18.0	19.0	(0.0 19.7)	C0.2
F1.3	(F1.4 17.7)	18.0	18.0	(F0.8 18.6)	F0.6
F1.0	F1.1 18.1	18.0	19.0	(F0.5 19.0)	F0.6
F0.2	(F0.3 19.3) ~~C0.3 20.2~~	19.4	21.4	(C1.2 21.6)	C1.4
F0.4	F0.6 18.9	19.5	20.6	(C0.7 20.6)	C0.9
C0.2	(0.0 19.7)	19.5	20.0	(C0.3 20.2)	C0.5
C1.1	C0.9 21.1	20.5	20.5	(C0.7 20.7)	C0.8
C1.2	C0.9 21.1	21.2	21.2	(C0.9 21.1)	C1.2
C0.3	(C0.2 20)	20.0	19.0	C0.2 20	C0.2

		1174.91		
⊙	2.50	1168.28	9.13	1165.78
39			5.32	1169.59
38			1.98 ~~3.86~~	1166.30
37			~~4.534~~	1162.94
36			7.36	1160.92
35			9.32	1158.96
34			9.94	1158.34
OBM			928	1159.00 1159.11
33	1.28	1160.39	2.67	1157.72
32			4.88	1155.51
31			8.68	1151.71
BM	0.18	1159.29		1159.11
30	.03 0.99	1147.92 1148.18	1149.01 1147.39 +0.3.1 .27	1147.91
29			3.88	1144.30
28			6.32	1141.86

F0.7	F0.9 18.4	18.2	18.7	(F0.5 19.0)	F0.2
F0.1	(F0.2 19.5)	19.5	21.5	(C1.2 21.7)	C1.3
C0.2	(0.0)	20.0	23.2	(C2.4 23.4)	C2.6
F1.8	(F1.7 17.3)	18.5	22.0	(F0.3 19.3)	C0.1
F2.0	(F2.0 16.8)	17.0	17.0	(F1.4 17.7)	F1.4
F2.1	F2.1 16.6	16.2	16.3	(F2.1 16.4)	F1.9
F1.9	F2.0 16.7	16.5	21.2	(C1.9 22.6)	C2.1
C0.2	C0.2 20	20.0	24.5	(C3.4 24.8)	C3.6
F0.9	(F1.0 18.3)	18.2	22.4	(C2.1 22.9)	C2.2
F0.1	(F0.3 19.3)	19.5	17.0	(F1.6 17.4)	F1.5
F1.5	(F1.5 17.5)	17.5	18.0	(F1.0 18.3)	F0.9
F1.0	(F1.0 18.3)	18.0	15 F 0	(F2.3 16.3)	F1.6

B.M.		1148.18	6.13	1102.05
27			8.74 / 8.13	1139.44
		1147.57		
26	1.21 / 0.99	1136.25	12.31	1135.26
			1.64	1134.61
25			6.26	1129.99
24			8.64	1127.61
23			9.83	1126.42
⊙	5.76	1133.06	8.95	1127.30
22			6.28	1126.85
BM	2.79	1083.02	2.79	1080.23 / 1080.23
21			4.97	1128.09
20			3.09	1129.33
19			2.45	1130.57
18			1.21	1131.81
⊙	5.25	1037.57	0.70	1032.32
17			4.52	1133.05
16+50			3.90	1133.67

Set plan

CO2	CO2 18	CO8 2-1 ← stake at 20'			
F1.1	(F1.4 17.6)	18.0	15.0	(F3.0 17.)	F2.2
F2.0	(F2.2 16.5)	16.0	17.0	(F1.7 17.9)	F1.0
F1.1	(F1.9 16.9)	16.5	18.7	(F1.5 17.5)	F1.2
F2.5	(F2.0 16.8)	17.0	F 14.0	(F2.0 14.2)	no manhole
F1.3	(F1.5 17.5)	17.5	21.2	(C1.8 21.7)	C1.5
C0.7	(C0.3 20.2)	20	21.0	(C1.2 21.2)	C1.3
F0.3	(F0.3 19.3)	18.5	19.2	(0.0 19.7)	C0.2
F1.6	(F1.5 17.5)	17.0	18.0	(F1.0 18.3)	F0.8
F1.3	F1.4 17.4	17.4	20.0	(C0.1 19.9)	C0.4
C0.4	C0.2 20.0	20.0	22.0	(C2.1 22.9)	C2.3

1137.51

16			3.22	1134.29				
15			2.60	1134.91				
14			3.22	1134.29				
13			4.46	1133.05				
12			5.62	1131.89				
0	5.18 mud	1136.86	(6.82)	1130.68				
11			4.58	1131.28				
10			4.35	1131.31				
9			3.88	1131.98				
8			2.68	1133.20				
0	3.90	1139.42	0.34	1135.52				
7			5.05	1134.37				
6			4.12	1135.30				
5			3.32	1136.10				

F0.4	(F0.5 19.0)	19.0	21.5	(C1.3 21.7)	C1.5
F1.7	(F1.6 17.4)	17.2	21.4	(C1.3 21.6)	C1.3
F1.7	(F1.8 17.1)	17.2	20.0	(C0.7 20.7)	C0.8
F1.0	(F1.0 17.5)	18.0	20.0	(C0.3 20.3)	C0.4
F1.2	(F1.2 18.0)	18.0	21.0	(C0.9 21.1)	C1.0
F2.2	(F2.1 16.6)	16.5	18.0	(F0.8 18.6)	F0.8
F2.1	(F2.3 16.4)	16.5	17.2	(F1.6 17.4)	F1.9
F1.2	(F1.4 17.7)	18.0	20.0	(C0.5 20.5)	C0.6
F0.5	(F0.6 18.9)	19.0	22.5	(C2.1 22.9)	C2.1
F1.0	(F1.0 18.3)	18.3	21.0	(C1.0 21.3)	C1.2
F1.5	(F1.6 17.4)	17.5	17.5	(F0.8 18.6)	F0.8
F2.1	(F1.9 16.9)	17.0	18.0	(F1.0 18.3)	F0.8

1139.42

4			2.52	1136.90
⊙	4.44	1141.17	2.74	1136.68
3			3.47	1137.70
2			3.18	1137.99
1475			3.61	1137.56
BM			4.02	1137.15
1			5.92	1135.25
⊙	1.39	1134.83	7.73	1133.49
⊙			~~9.17~~ 2.83	1132.00

F1.7	(F1.6 17.4)	17.2	19.0	1-1 C0.7 19.2	C1.0
F1.1	(F1.1 18.1)	18.0	20.1	1-1 C2.6 20.5	C2.3
F1.6	(F1.6 17.4)	17.2	20.0	C1.4 1-1 19.9	C1.7
F0.7	F0.9 18.4	18.2	20.5	1-1 (C2.0 20.5)	C1.4
C0.8	(1-1 C0.6 19.1)	19.2	20.1	1-1 (C2.6 21.1)	C3.0
C0.9	1-1 C0.6 18.1	19.0	20.0	C1.5 20.0	C1.7

MAY-16. 1922 FORM STAKES
LACKER
GRAU
PHILLIPS

	109	1085.84		1084.75	spike side of Apple
260 +50			6.12	1079.72	
260			7.04	1078.80	
259+50			7.96	1077.88	
259 +75			8.88	1076.96	
258+50 +25			9.75	1076.09	
258 0+75	1.77	1077.08	10.53 (1053)	1075.31 (1075.31)	
7 +50			2.46	1074.62	
+25				1074.80	
257			3.06	1074.02	
+50			3.61	1073.47	
+25					
256			4.06	1073.02	
+75					
+50			4.28	1072.80	
255			4.11	1072.67	

1077.08

254+50			4.53	1072.55
254			4.66	1072.42
+50			4.78	1072.30
⊙	3.69	1075.99	4.78	1072.30
253			3.82	1072.17
BM +75			2.45	1073.54
+50			3.90	1072.09
+25				
252			3.91	1072.08
+75				
+50			3.83	1072.16
+25				
251			3.67	1072.32
+50			3.47	1072.52
250			3.27	1072.72
+75				
+50			2.90	1073.09
+25				
249			2.19	1073.80
⊙	6.58	1080.38	2.19	1073.80

48 + 69.60
246 + 77.95
1 91.65

1080.38

PT +69.60				
+75				
+50			5.54	1074.84
+25				
248			4.16	1076.22
+50			2.61	1077.77
+25				
247			1.38	1079.00
+77.95				
+75				
246+50			1.78	1078.60
+25				
246			3.64	1076.74
+50			5.31	1075.07
245			6.31	1074.07
⊙	5.30	1079.01	6.67	1073.71
44+50			~~6~~5.29	1073.72
244			4.97	1074.04
243+50			4.32	1074.69
243			3.67	1075.34
+50			3.02	1075.99

~~1079.00~~

78.60

1077.77	76.74
1076.22	75.07
1.55	1.67

78.60	2.54
76.74	1.86
1.86	4.40
	1.67
	6.07

79.00
77.77
1.23

5.62
1.55
4.07
1.23
2.84

X

+69.60	57'-29"
+50	54'-33
248	47'-03"
+50	39'-33"
247	32-03
+50	24'-33"
246	17'-03"
+50	4'-03"
245	2'-3"

PC = 44+86.27

N.W. COR of E HWALL OF PIPE
PC

MAY 17. 1922
LACKEY
GRAU
PHILLIPS
1079.01

242			2.37	1076.64	
+50			1.72	1077.29	
241			1.07	1077.94	
0	6.94	1084.88	1.07	(1077.94)	
BM +50			6.29	1078.59	
BM			4.53	1080.35	
240			5.64	1079.24	
+50			4.99	1079.89	
239			4.34	1080.54	
+50			3.69	1081.19	
238			3.13	1081.75	
+50			2.76	1082.12	
237			2.49	1082.39	
0	5.22	1087.61	(2.49)	(1082.39)	87.49
+50			4.94	1082.67	
236			4.67	1082.94	

31

1077.94
6.94
1084.88
6.24
1078.59

67
8239
.28

503
.28
4.75
4.48
.30
4.18

47.5
4.47
4.48
.12
4.60
4.18
.12
4.30

1080.41
3.88
1084.29

1080.41

1084.29				
3.75 / .12 / 3.87				
3.10	3.08 / .12 / 3.20			
2.54	3.48 / 3.60			
2.17	2.12 / .12 / 2.24			
1.90	1.82 / .12 / 1.95	~~87.49~~	195	8234 / 875 / 8749
4.82				

108761

235+50		4.37	108324	8749 .2
235		4.03	108358	3.91
+50		3.64	108397	3.52
234 (vert PI)		3.22	108439	3.10
+50		2.74	108487	2 62
+00.25 PT 6.47	⊙ 1089.70	438	1083.23	
233	MAY 18, 1922	4.32	1085.38	2 11
	LACKEY			
(232+75)	GRAU PHILLIPS	~~3.87~~	108583 .66	1.83
232+50		3.76	108594	1.50
				92.80
232+25		3.53	1086.17	6.63
232+0		3.16	108654 3	6.26 92 35
231+75		2.85	1086.85	
231+50		2.53	1087.17 3	5. 18
231+25		2.22	108748	4 87

4.25

384 .12 3.96

3.44 .12 356

302 .12 3.14 254 .12 2.66

3.44 .42 3.02 48 254

9237 8634 3.81

Top Stump 50. R 234+50

205 2.01

173 .21 1.52

8749 .125 8624 656 6580 9280

173 28 145

145 21 124

145 145

8744 .125 86.24 6.56 9280

92.80 8617 13

92.80 8634 626 6 31

650 21 629

620 21 599 5.89

620 21 599 21 5.68

599 31

9280 247 90.33 culvert 203 92.3

547 32 5.87 21 5.36

on 513 21 492 4.72 21 451

		108970					
231			1.91	108779	92.35	4.56	450 429
⊙	6.24	1094.03	(1.91)	(1087.79)			
230+75			5.93	1088.10	~~4.25~~	4.17	3.98
230+50			5.61	1088.42	3.93	3.87	3.66
230+25			5.30	1088.73	3.62	3.56	3.35
230+0			4.99	1089.04	3.31	3.25	3.04
229+75			4.68	1089.35	3.00	2.94	2.73
+50			4.36	1089.67	2.68	2.62	2.41
+25			4.05	1089.98	2.37	2.31	2.19
229			3.74	1090.29	2.06	2.00	1.79
+75			3.43	1090.60	1.75	1.69	1.48
+50			3.11	1090.92	1.43	1.37	1.11
+25			2.80	1091.23	1.12	1.06	.85
⊙			~~0.86~~		92.35	91.49	

109402

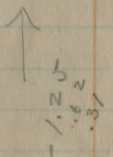
+09.20 △PI

229

+75

+50

+25



228			2.49	109154	6.28	
⊙	7.44	109898	(249)	1091.54		
+75			7.13	1092.85	5.97	
+50			6.81	1092.17	565	
+25			6.50	1092.48	534 ~~530~~	
227 V.PT			6.19	109279	503	
+75			5.86	109312	470	
+50			5.96	109352	430	
+25			4.96	109402	~~491~~ 380	

WI 9782		
622	6.01	
5.91	5.70	
5.59	5.38	
5.28	5.07	
497	476	
464	923	
424	403	
374	353	

PC 225+16.92

	+25	2°-25"
	+50	9°-55"
	+75	17°-25"
226		24°55"
	+25	32°-25"
	+50	39°-55"
	+75	47°-25"
227		54°-55"
	+25	1°02°-25"
	+50	1°-9°-55"
	+75	1°-17°-25"
228		1°-24°-55"
	+25	1°-32°-25"
	+50	1°-39°-55"
	+75	1°-47°-25"
229		1°-54°-55"
	+25	2°-02°-25"
	+50	2°-09°-55"
	+75	2°-17°-25"
230		2°-24°-55"
	+25	2°-32°-25"
	+50	2°-39°-55"
	+75	2°-47°-25"
231		2°-54°-55"

	1098.98			
226 ⊙ 1094.04		4.55	1094.43	
+75		3.95	1095.03	
+66.92 End of run off				
+50		3.44	1095.54	-.27 +15
+25		2.82	1096.16	.19 +07
0		(2.83)	1096.15	
+16.92 PC				
225 PC Vert			1096.84	.11 = -.01
BM +66.92		2.97	1096.01	1096.12 / 8.30 / 1104.42
224+50			1098.24	
224			1099.64	~~4.78~~
+50			1101.04	
+25 PT			1101.82	
223			1102.52 ⊙	1.90 / 1102.52 / 12.53 / 1115.05
+75 ⊙			1103.45	
+50			1104.55	
+25 PC			1105.70	
222			1107.12	

~ BM 1.74

97.82 / 1.74 / 96.08 BM

97.82				
			231+25	3°-02'-25"
3.39	3.33 / 2.12		+50	3°-09'-55"
			+75	3°-17'-25"
2.79	2.73 / .52		232	3°-24'-55"
			+25	3°-32'-25"
2.28	2.22 / 2.07		+50	3°-39'-55"
			+75	3°-47'-25"
1.66	1.60 / 1.58		233	3°-54'-55"
			+02.5	3°55'
	97.82	96.12 / 1.74 / 97.86 / .92 / 96.94 correct	1096.12 / 8.30 / 1104.42	
0.98	.92 / HI 96.90			1104.42 / 96.84 / 7.58
HI 96.94				
5.18			1104.42 / 98.24 / 6.18	7.54
4.78				
3.38				
1.90				
10.50				
7.43				

		111505			~~1778.08~~
+50			5.28	1109.77	
221			2.63	1112.42	
0	12.60	1125.01	(2.64)	(1112.41)	
+50			9.94	1115.07	
220			7.29	1117.72	
+50			4.64	1120.37	
219			1.99	1123.02	
⊙	12.93	1135.95	(1.99)	(1123.02)	
+50	5.37%		~~.54~~ 10.28	1125.67	
218			7.63	1128.32	
+50			4.98	1130.97	
217	PT		2.33	1133.62	
+75				1134.92	
+50	(TP) 5.52	1141.31	.15 0.16 1.71	1135.80 (1135.79) 1139.60	1139.64
	2.10	1141.74			
+25 ⊙				1136.53	
216	+0.47%		4.71	1137.03	
+75			.46	1137.28	

2.10

1141.74
35.80
594

		1141.74	
215+50 PT	+0.47%		
+25		4.44	1137.30
			1137.26
215 0		4.38	1137.36
			1137.59
+75			
+50 PC		3.79	1137.95
214	1.7	2.94	1138.80
+50		2.09	1139.65
			1140.08
213 PT		1.24	1140.50
+75			1140.87
+50		.61	1141.13
+25			1141.28
212		A2	1141.32
+75	1.26 TP 1142.58	OUD	1141.26
+50		1.50	1141.08
+25			1140.80
211 PC *		2.18	1140.40
+50		3.08	1139.50
210	+1.8	3.98	1138.60
+50		4.88	1137.70

PC = 211+10

211+25	0° 9'
+50	0°-24'
+75	0°-39'
212	0° 54'
+25	1°-09'
+50	1°-24'
+75	1°-39'
213	1°-54'
+25	2°-09'
total	2°-10-30

PI = 212+188

Δ = 4°-21 L

2°-

L = 217.5

Ex 2.07

PT = 213+27.5

1142.54

209		5.78	1136.80	
+50	PT x	6.68	1135.90	
+25			1135.58	
208 ⊙		7.33	1135.25	
+75			1135.13	
+50	P.T.x	7.46	1135.12	
207		7.35	1135.23	
+50		7.24	1135.34	
+25	PT	[illegible]	1135.40	
206		7.25	1135.33	
+75 ⊙			1134.99	
+50		8.19	1134.39	
	TP	(8.19)	1134.39	
+25	TPC	1138.29	1133.52	
205		5.77	1132.52	1132.52

1134.78
3.51
1138.29
3.85
1134.44

5.72
3.85
1.87

HI 1140.54

	0	1138.29				
+50	PT.			7.77	1130.52	1130.90
+25					1129.69	
204 △				8.99	1129.30	1130.07
+75					1129.24	
+50 N	PC + PT			8.67	1129.62	1130.00
N	TP 8.47	37.96		8.80	29.49	
203	PT			7.24 [crossed out]	1130.72	1030.72
+75					1131.31	
+50				6.10	1131.86	[crossed out]
+25					1132.76	
202 △				4.89	1133.07	1132.92
+75					1133.76	
+50				3.59	1134.37	
+25					1135.04	
201	PC.			2.22	1135.74	
+50 N	(TP) 7.96	43.71		(3.21) 6.56	35.75 1137.15	
200				5.15	1138.56	
+50				3.74	1139.97	
199				2.33	1141.38	
+50				.92	1142.79	(42.67)
198	(TP) 9.59	52.26		(0.94) 8.06	1144.20	
+50				6.65	1145.61	
197				5.24	1147.02	
+90	P.T.				1147.30	

847

on Sand of E Head wall of Pipe

2949
847
3796
2962
834

61
524
88

	N / A / N.	5236	Rds +0.1	sound off 0.1	
196+75	1		~~1.58~~	1147.68	
+50	+40△		4.09	1148.17	1148.71
+25				1148.32	
196	b		3.73	1148.49	
+90	o PC			1148.44	
+50	x		4.00	1148.26	✓
	TP	3.74 5204 ~~51.99~~	4.01	(48.25)	48.35
195	+PT		3.98	1148.01	✓
+75				47.90	
+50	b		4.16	1147.83	✓
+25	o			47.79	
194	x		4.20	1147.79	✓
+75				47.83	
+50			4.09	1147.90	
+25				48.01	
193	△		3.84	1148.15	1147.01
+75				1148.34	
+50	b		3.45	1148.54	
+25	x			1148.79	
192	1		2.92	1149.07	∠TP
+75				1149.46	
+50				1149.75	
+25				1150.14	
191	PC +PT			1150.57	

3.37
2.34

0.91

42.67
9.60
52.27
.91
51.36

3.56 on S.E. Cor of S.) head wall
48.43

190+75	[illegible]	1151.04	
+50	Δ	1151.81	1151.46
+25		1152.63	
190	PC	1153.76	
+50		1156.06	
189		1158.36	
+50	N PT	1160.66	
+25		61.78	
188		1162.85	
+75		63.77	
+50	Δ	1164.81	1165.26
+25		66.25	
187		1166.55	
+75		67.33	
+50	PC	1168.06	
186		1169.46	
+75			
+50		1170.66	✓
+25		1171.11	
185		1171.46	

65.7° N I

[illegible] – 187+50
[illegible] fence

36
1165.34
6.97
1172.31

+75	2·1	1171.71	
+50	△	1171.86	
+25		1171.91	
184		1171.86	×
+75	0 2 ×	1171.71	
183+50	⊕	1171.46	
+25		1171.11	
183.+		1170.66	
+50 PT			
+25		1169.66	
182	△	1168.89	
+75			
181+50 PC		1168.58	
~~+25~~			
181		1168.50	
+50		1168.42	
180	+.4	1168.34	
+50		1168.26	

1172.3' HI
7.72
71.59
3.99
75.58
7.25
68.33
.376
72.09

6833
436
7269

m ~~?~~ NE
?E. on head wall

183+46.79 PC
185+26.79 PT =
1°
1-48 R

183+50	58'
+75	8°-28'
184+0	15°-58
+25	23°-28'
+50	30-58
+75	38-28
185	45.58
+25	53-28
+26.79	32
	54-0'
	2
	108'0
	1°48

Station			Elevation	
179			1168.18	
178+50			1168.10	
178		0.87	1168.02	67.98
+50		x	1167.94	67.88
177+25 = PT			1167.90	67.68
177			1167.78	67.33
+75	1.0	70	1167.47	66.87
+50	x	73.00	1167.03	66.35
+25	5.Δ	x	1166.32	65.61
176	5	x	1165.59	64.87
+75	+	x	1164.61	64.02
+50		x	1163.50	63.06
+25	PC	x	1162.20	61.96
175			1160.82	60.7
~~+75~~				1158.44
+50			1158.07	
~~+25~~				
174			1155.31	
+50			1152.55	
173			1149.79	
+50			1147.03	
172			1144.76	

Changed from 200' Vert

1172.04
10.27
62.42
1.57
63.99
11.53
52.46 Elev

1173+50

52.46
0.29
52.75
~~11~~
8.06
44.69

Δ = 2°-34' L
D = 1°00
T = 1.28.26
PC = 174+95.34
PT = 177+52.01

175	1°-	24"
+25	8°-	54"
+50	16°	24"
+75	23	54
76	31	24
+25	38	54
+50	46	24
+75	53	54
177	1-01	24
+25	1°-8'	54
+50	1° 16'	24
+52.01	1° 17'	00

4~~4~~.69 on a parapet
323
4~~4~~ 92 HI

17~~1~~+50				1143.46
171				43.15
+50				43.81
170				44.96
+50				46 11
169				47.50
⊙	11.55	58.93	(0.54)	(47.38)
+50			9.69	49.36
168			7.59	51.46
+50			5 37	53.56
167			3.27	55.66
+50			1 17	57.76
⊙	11.66	1169.30	(129)	57.64
166				59.86
+50				61.96

6930

165			424	1164.06
+50				66.16
⊙	9.68	76.26	2.72	66.54
164				68.76
+50				70.31
163				71.99
+50		lowered .15 on N side for run off		73.27
162				74.10
~~+87.73~~ PC				~~74.34~~
161+50		1178.41 HI		1174.34
161+0				1173.94
160+50				1172.91
160+0				1171.34
159+50				1169.69

74.73
1.78
72.54

4°
Δ = 13°20 L
PI 164+55.15
PC = 162+87.73
PT = 166+21.06
L = 333.33

162+87.73	
163	14 43
+25	44.43
+50	1 14.43
+75	1 44.43
164	2 14.43
+25	2 44.43
+50	3 14.43
+75	3 44.43
165	4 14.43
+25	4 44.43
+50	5 14.43
+75	5 44.43
166	6 14.43
+21.06	25 16
	6-40-00
	2
	13°20 L

		HI			
		1178.41			
159				1168 04	
158+50				1166.39	
0	0.12	1166.39	(12.14)	(1166 27)	
158				1164.74	
157+50				1163.09	
157+0				1161.44	
156+50				1159.79	
156				1158.14	
55+50				1156.49	
	0.90	57.27	10.02	(56.37)	
155				1154.84	
154+50				1153.19	
154				1151.64	
153+50				1151.09	
TBM			12.23	1150.11 RR / 1150.04	Blue on Rt. Pav.

9.21-'22 Hanna
110.+ Gray
Fair

B.M.	1.12	1131	35			1130.23
20+50					2.64 / 2.68	28.71
21					3.26 / 3.30	28.09
+50					3.88 / 3.92	27.47
22					4.50 / 4.54	26.85
+50					4.92 / 4.96	26.43
23					4.93 / 4.97	26.42
+50					4.54 / 4.58	26.81
24					3.74 / 3.78	27.61
+50					2.74 / 2.78	28.61
25					1.36 / 1.40	29.99
T.P.	11.80	1141	75		1.40	1129.95
+50					9.64 / 9.68	32.11
26		(Low)	7.21		7.14 / 7.18	34.61
+L.C.		(Low)	(5.73)		5.86 / 5.90	35.89
B.M.					1.41	40.33 / 1140.34
+50		(Low)	(4.75)		4.64 / 4.68	37.11
B.M.	3.92	1134	15			1130.23
20					4.82 / 4.86	29.33
+50					4.20 / 4.24	29.95
19					3.58 / 3.62	30.57
+50					2.96 / 3.00	31.19
18					2.34 / 2.38	31.81
+50					1.72 / 1.76	32.43
17					1.10 / 1.14	33.05
T.P.	4.87	1137	88		1.14	1133.01

37.88
33.05
4.83
4.87

153	1151.77
152+50	1153.67
152	1156.70
151+50	1159.95
151+0	1163.20
150+50	1166.45
150	1169.70
149+50	1172.95
149	1176.12
148+50	1178.76
148	1180.79
147+50	1182.20

		1137 88		
+50			4.21 / 4.25	33.67
16			3.59 / 3.63	34.29
+50			3.13 / 3.17	34.75
15	3.00		2.97 / 3.01	34.91
+50			3.13 / 3.17	34.75
14			3.59 / 3.63	34.29
+50			4.21 / 4.25	33.67
13			4.83 / 4.87	33.05
+50			5.45 / 5.49	32.43
12			5.99 / 6.03	31.89
T.P.	3.65	1135 50	6.03	1131.85
+50			3.99 / 4.03	31.51
10			4.22 / 4.26	31.28
+50			4.28 / 4.32	31.22
Temp. B. M. E. Para Culv.			4.25	1131.25
10			4.19 / 4.23	31.31
+50			3.93 / 3.97	31.57
9			3.52 / 3.56	31.98
+50			2.95 / 2.99	32.55
8			2.30 / 2.34	33.20
+50			1.68 / 1.72	33.82
7			1.13 / 1.17	34.37
+50	(Omit this distance)	(0.16 Low)	0.63 / 0.67	34.87

147	1183.08
146+50	1183.88
146	1184.68
+50	1185.41
145	1186.00
+50	1186.46
144	1186.78
+50	1187.03
143	1187.28
+50	1187.56
142	1187
+50	
141	

BM 421 // 41.39 1137.18

0	9.37 / 9.43	✓	32.00
+50	7.76 / 7.80	✓	33.63
1	6.14 / 6.18	✓	35.25
+50	4.51 / 4.55	✓	36.88
2	3.40 / 3.44	✓	37.99
+50	3.28 / 3.33	✓	38.10
3	3.62 / 3.73	✓	37.70
+50	4.03 / 4.13	✓	37.30
4	4.39 / 4.53	✓	36.90
+50	4.87 / 4.93	✓	36.50
5	5.29 / 5.33	✓	36.10
+50	5.67 / 5.73	✓	35.70
6	6.09 / 6.13	✓	3530
+50	6.52 / 6.56	✓	34.87

End

140+50

140

139+50

139

+50

138

+50

137

+50

136

+50

135

+50

134

+50

133

+50

132

+50

131

+50

130

+50

129

+50

128

+50

127

+50

126

+50

125

+50

124

+50

123

+50

122

+50

121

+50

120

+50

119

+50

118

+50

117

+50

116

+50

115

+50

114

+50

113

+50

112

+50

111

+50

110

+50

109

+50

108

+50

107

+50

106

+50

105

+50

104

+50

103

1187.35 BM on Locust
2.33
1189.68 HI
10.07 FS

~~1179.75~~
1179.61
3.27
1182.88 HI
11.45
71.43 elev
1.11
1172.54
12.64
1159.85
8.54
1160.39
8.08
1152.31

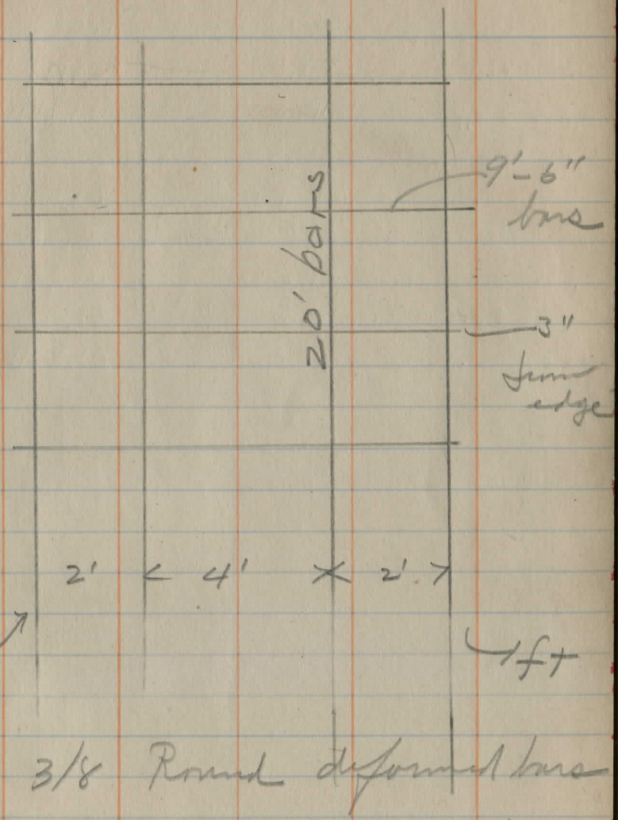
stakes set out 15.5 - ℄ ft E of ditch

Pipe 148+60 To 150+60

148+25 Δ	Profile Grade	HI 1182.88	Profile Rd	d. rod	
148+50	1178.76		=		
+60	1178.20		4.68 + 2.5 =	7.18	3.18 c 4.0
149	1176.12		6.76	9.26	3.26 c 6.0
+25 = PT					
+50	1172.95		9.93	12.43	5.43 c 7.0
150	1169.70	72.54	13.18	15.68	8.18 c 7.5
+50	1166.45		6.09	~~8.59~~	3.54 ~~c 5.0~~
+60	1165.80		6.74	9.24	3.74
				3.74 c 5.50 on +60	

+50 omitted

63.20



3/8 Round deformed bars

5-340. bars 20' long
17. 374 bars 9'-6" long
103304# ±

32 × 30ft □

260 +75	Spike in SW side 12" Apple	1084.75
252+90	Staple SW Root 14" M R	1073.56
240+10	" S E " 12" CHERRY R	1080.41
226+95	" E root of 12" Maple L	1096.12
215+90	" N.W root Map. 12" R	1139.64
206+25	" S.E. Root 10" Maple L	1134.78
197	" N.W Root 12" WAL. R	1151.53
184	" S.E Root 24" P. Hick. L	1172.81
162+10	" N.W. Root 14" M R	1174.73
144+50	" S E Root 18" Locust L	1187.35
121+75	" W. Root 30" Elm R	1196.66
125+14	" W Root 12" M. 26' R	1210.91

$1\frac{1}{2}'' = 7\frac{1}{2}$ $\frac{3}{2} \times \frac{1}{12} = \frac{3}{24} =$

130 × 1.25

1151.53
1.8.9
1153.42

1151.53
1.8.9
1153.42
4.83
1148.59
12.43
1161.02
1.21
1059.81
13.07
5.64

1059.71
13.07
1072.78
.90
1071.88
3.24
1075.12
3.20
1029.2

73
48
25

1072.81
3.21
1010.2

154 T. BM. S.W. Cor W Parapet 1152.33

1072.81
3.21
1076.00
7.93
1068.07

1072.81
3.21
1076.02

1151.53
2 31
1153 84
5 2 4
1148 60
13 08
1161 68
1 8
1159 84
12 93
1172 77
0 26
1172 51 on top pg
5 05
1177.56 F S on BM
4 72
1172.84

1177.56
71.46
6 10
3 90
2.2
180 Bml

77.56

1177.46
71.38
1

1177.56

184
77.56
71.86
5.70

34.15
28.71
5.44

1153.84
48.01
5.82

73.0
5.8
1.5

71.46

1161.68
53 76
7 92

9.5
7.9
1.6

1172.77
69 46
3.21

172.77
66 55
6.22
5.62
60

1172 17
66 55
5.62

7.00
5.62
F 14

10770
+75
1077.56
71.91
Bml 5.65

117.277
69.46
3.31
2.4
0.9

57
32
25

1072.51
1071.46
1.05

1.05
26
79

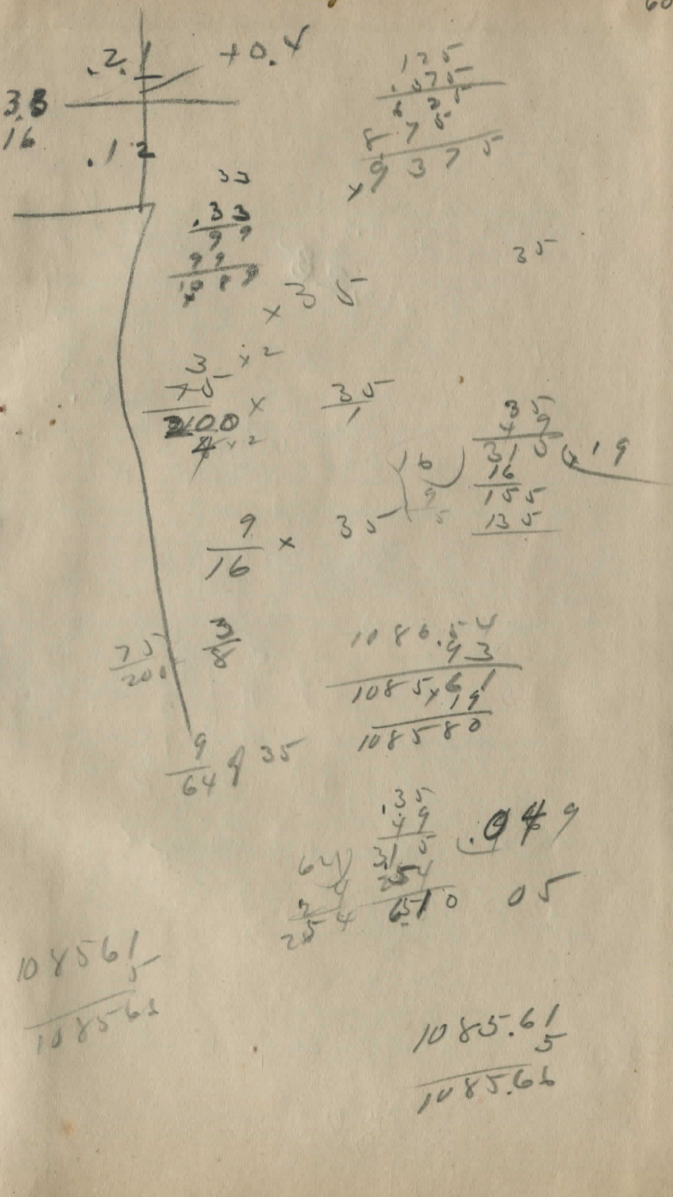


TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
[illegible]	[illegible]	[illegible]	.1927	[illegible]	.2969	[illegible]	.4010	[illegible]	.5052	[illegible]	.6094	[illegible]	.7135	[illegible]	.8177	[illegible]	.9219		
[illegible]	[illegible]	[illegible]	.1979	[illegible]	.3021	[illegible]	.4063	[illegible]	.5104	[illegible]	.6146	[illegible]	.7188	[illegible]	.8229	[illegible]	.9271		
[illegible]	[illegible]	[illegible]	.2031	[illegible]	.3073	[illegible]	.4115	[illegible]	.5156	[illegible]	.6198	[illegible]	.7240	[illegible]	.8281	[illegible]	.9323		
[illegible]	[illegible]	[illegible]	.2083	[illegible]	.3125	5—	.4167	[illegible]	.5208	[illegible]	.6250	[illegible]	.7292	10—	.8333	[illegible]	.9375		

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250 X

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
DRAWING MATERIALS AND SURVEYING INSTRUMENTS